

On the Property and Configuration of the Short Time DFT Hilbert Transformers

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Short Time DFT を用いた Hilbert 変換器の特性と構成

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Hilbert transformers have been previously studied with putting emphasis upon signal processing [1], as they are inevitable in preventing such modulation as single side band (ab. in SSB) or RZ SSB [2] from increasing frequency bandwidth over radio channels.

By adopting instantaneous spectrum analysis, namely "ST-DFT" (short time Discrete Fourier Transform, ab. in ST-DFT), a novel realization of Hilbert transformers is proposed in this paper and successfully examined to be free from errors via computer simulations.

1. INTRODUCTION

It is unfortunate that existing Hilbert transformers have been realized to possess phase shifting function by approximate $\pi/2$ radian from the point of view for all-pass filter. On the other hand, ST-DFT Hilbert transformers proposed here are based on the instantaneous spectrum analysis [3]. Where the instantaneous spectrums are given, Hilbert transform is precisely carried out via merely exchanging real or imaginary part of these spectrums with each other. Hilbert transformed output signals are, therefore, synthesized via inverse ST-DFT (ab. in ST-IFT) from the interchanged instantaneous spectrums.

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A circuitry configuration of the ST-DFT Hilbert transformer is categorized into three major blocks, namely, I instantaneous spectrum analyzer, II frequency domain Hilbert transformer, III output signal synthesizer. It is easy to understand that the ST-DFT Hilbert transform is ideal and free from any distortion, while the instantaneous spectrum analysis is performed without any errors.

2. INSTANTANEOUS SPECTRUM ANALYSIS AND SYNTHESIS

Consider first how the ST-DFT gives the instantaneous spectrum and what characteristic it possesses. Let instantaneous spectrum $\Phi(n)$ at sampling time n be described by,

$$\Phi(n) = \{ \phi_0(n) \ \phi_1(n) \ \phi_2(n) \ \cdots \ \phi_{N-1}(n) \}^T. \quad (1)$$

Where, $\phi_k(n)$ is a spectrum component at frequency index k of $\Phi(n)$ given as,

$$\phi_k(n) = \sum_{r=-\infty}^{\infty} x(r) h(n-r) W_N^{-rk}, \quad (2)$$

$$W_N^{-rk} = \exp\{-j(2\pi rk/N)\},$$

integer k is $0 \leq k < N$.

Here, $x(r)$ is an input data at sampling time r . W_N^{-rk} is the same operator defined as that of existing DFT.

Existence of ST-DFT requires that output signal $y(n)$ at time n is precisely produced from the instantaneous spectrum $\Phi(n)$ via ST-IFT. That is,

$$y(n) = \sum_{k=0}^{N-1} \phi_k(n) W_N^{nk}, \quad (3)$$

$$W_N^{nk} = \exp\{j(2\pi nk/N)\}.$$

Here, W_N^{nk} is the same operator as existing inverse DFT.

The ST-IFT denoted by eq.3 requires that the window function $h(p)$ of eq.2 holds condition $y(n) = x(n)$. Substituting eq.2 into eq.3 and exchanging the summation order for variables k and r , it gives eq.4.

$$y(n) = \sum_{k=0}^{N-1} \left\{ \sum_{r=-\infty}^{\infty} x(r) h(n-r) W_N^{-rk} \right\} W_N^{nk}$$

$$= \sum_{r=-\infty}^{\infty} x(r) h(n-r) \left\{ \sum_{k=0}^{N-1} W_N^{(n-r)k} \right\}. \quad (4)$$

The summation for variable k takes non zero value by N , only if $n-r=2Nq$. Here, q is an integer. This gives a restrict condition to the window function as follows,

$$h(p) = \begin{cases} 1, & \text{if } p = 0 \\ 0, & \text{if } p = 2Nu, \\ & u \text{ is non zero integer.} \end{cases} \quad (5)$$

For example, an N frame length Nyquist window function truncated with $2m$ frame number

$h(p)$,

$$h(p) = \frac{\sin(p\pi/N)}{(p\pi/N)}, \quad (6)$$

$$-mN \leq p \leq mN,$$

are able to satisfy eq.5. Hereafter, the truncated Nyquist will be employed for the present as a window function in the ST-DFT.

3. PRINCIPLE OF ST-DFT HILBERT TRANSFORMERS

Figure 1 shows the processing outline in the ST-DFT Hilbert transformer. As being discussed in previous section, input signal $x(r)$ is at first in the ST-DFT Hilbert transformer analyzed by ST-DFT to yield instantaneous spectrum $\Phi(n)$. Secondly, both real and imaginary parts of each component of the instantaneous spectrum are exchanged with each other to get Hilbert transformed spectrum $\hat{\Phi}(n)$. Output signal $\hat{y}(n)$ is finally synthesized through ST-IFT from the transformed spectrum.

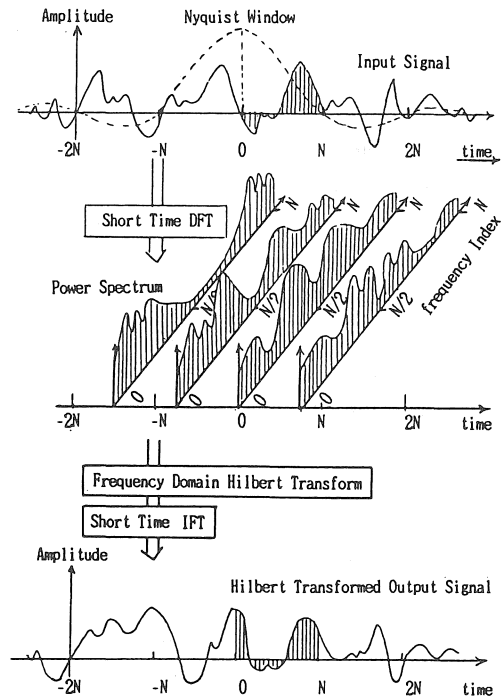


Fig.1 Processing Outline in the ST-DFT Hilbert Transform

Both instantaneous spectrum analysis and phase shifting being combined into one operator, the frequency domain Hilbert transform operator \widehat{W}_N^{-rk} is given as follows,

$$\widehat{W}_N^{-rk} = \begin{cases} \exp\{-j(2\pi rk/N + \pi/2)\}, & \text{if } 0 < k < N/2 \\ 0, & \text{if } k = 0, N/2 \\ \exp\{-j(2\pi rk/N - \pi/2)\}, & \text{if } N/2 < k < N. \end{cases} \quad (7)$$

Here, j is complex unit, $j = \sqrt{-1}$.

Proof: Existence of Frequency Domain Hilbert Transform Operator

Constant $\pi/2$ on the first row of eq.7 gives features of phase shifting function by $\pi/2$ radian to the k -th component $\phi_k(n)$ of $\Phi(n)$. This also clearly shows that the frequency domain Hilbert transform is free from amplitude distortion, because operator \widehat{W}_N^{-rk} consists of single complex exponential function only with pure imaginary variables.

Both the second and third rows of eq.7 satisfy that $\widehat{y}(n)$ exists physically. Substituting $\widehat{\phi}_k(n)$ with $\phi_k(n)$ of eq.3, $\widehat{y}(n)$ is given as follows,

$$\begin{aligned} N \cdot \widehat{y}(n) &= \sum_{k=0}^{N-1} \widehat{\phi}_k(n) W_N^{nk} \\ &= \widehat{\phi}_0(n) W_N^0 + \widehat{\phi}_{N/2}(n) W_N^{nN/2} \\ &\quad + \sum_{k=1}^{N/2-1} \{ \widehat{\phi}_k(n) W_N^{nk} + \widehat{\phi}_{N-k}(n) W_N^{n(N-k)} \} \end{aligned} \quad (8)$$

In eq.8, W_N^0 or $W_N^{nN/2}$ takes pure real 1 or $1(-1)$, respectively. If $\phi_0(n)$ or $\phi_{N/2}(n)$ is non zero, the corresponding transformed component $\widehat{\phi}_0(n)$ or $\widehat{\phi}_{N/2}(n)$ takes pure imaginary value and the output $\widehat{y}(n)$ diversifies to complex. So \widehat{W}_N^{-rk} has to vanish at $k=0$ and $N/2$ as defined in eq.7.

Since $W_N^{n(N-k)}$ is given by complex conjugate with W_N^{nk} , i.e. $W_N^{n(N-k)} = \overline{W_N^{nk}}$,

every bracketted term of eq.8 takes a pure real number, if and only if $\widehat{\phi}_{N-k}(n)$ is complex conjugate with $\widehat{\phi}_k(n)$. In practice, $\widehat{\phi}_{N-k}(n)$ is given as

$$\begin{aligned} \widehat{\phi}_{N-k}(n) &= \sum_{r=-\infty}^{\infty} x(r)h(n-r) \exp\{-j(2\pi r(N-k)/N - \pi/2)\} \\ &= \sum_{r=-\infty}^{\infty} x(r)h(n-r) \exp\{j(2\pi rk/N + \pi/2)\} \\ &= \overline{\widehat{\phi}_k(n)}. \end{aligned} \quad (9)$$

Therefore, the output $\widehat{y}(n)$ becomes pure real number as follows,

$$\begin{aligned} N \cdot \widehat{y}(n) &= \sum_{k=1}^{N/2-1} \{ \widehat{\phi}_k(n) W_N^{nk} + \widehat{\phi}_{N-k}(n) W_N^{n(N-k)} \} \\ &= \sum_{k=1}^{N/2-1} \{ \widehat{\phi}_k(n) W_N^{nk} + \overline{\widehat{\phi}_k(n)} \overline{W_N^{nk}} \} \\ &= \sum_{k=1}^{N/2-1} 2 \text{Real}\{ \widehat{\phi}_k(n) W_N^{nk} \}, \quad \text{QED.} \end{aligned} \quad (10)$$

4. CIRCUITRY CONFIGURATION AND ITS UNIT SAMPLE RESPONSE

Figure 2 shows a primitive block diagram of ST-DFT Hilbert transformers. ST-DFT Hilbert transformers are categorized into three major functional blocks.

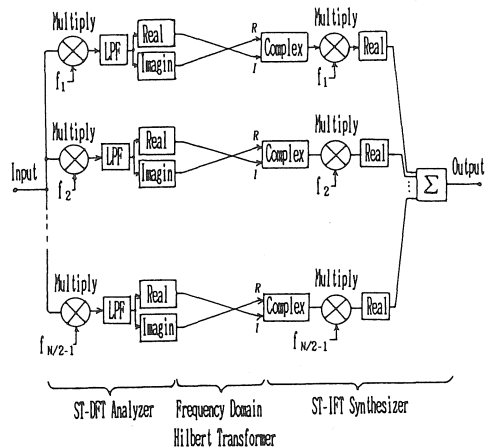


Fig.2 Configuration of the ST-DFT Hilbert Transformer

The first functional block plays a role of ST-DFT analyzers and consists of $N/2-1$ channel modules in which every component $\phi_k(n)$ of the instantaneous spectrum $\Phi(n)$ is yielded, here $k=1, 2, \dots, N/2-1$. Inner product of $x(n)$ and W_N^{-rk} in eq.2 is performed of modulating the input $x(n)$ with complex carrier W_N^{-rk} of $2\pi k/N$ normalized angular frequency. Convolution $\{x(r)W_N^{-rk}\}$ and $h(n-r)$ in eq.2 is also interpreted as low-pass filtering for modulated signal $\{x(r)W_N^{-rk}\}$.

The second block acts as a Hilbert transformer on the frequency domain, which exchanges the real with the imaginary part of $\phi_k(n)$. This block is dominant in function, however, its circuitry configuration is so simple as it only possesses two crossing wires as shown in fig.2. The first and second blocks are practically combined together in frequency index wise to get $\hat{\phi}_k(n)$ directly by

adopting \hat{W}_N^{-rk} instead of W_N^{-rk} during the modulation.

The last is synthesizer which employs ST-IFT to produce time domain signal from Hilbert transformed spectrum $\hat{\Phi}(n)$.

In similar to the first block, ST-IFT is performed of modulating Hilbert transformed spectrum component $\hat{\phi}_k(n)$ with complex carrier W_N^{rk} of $2\pi k/N$ normalized angular frequency.

An unit sample response $I_s(n)$ of the ST-DFT Hilbert transformer is given in eq.11 by using eqs.6, 7 and 8 when the unit sample $x(n)$ is taken to be $x(0)=1$.

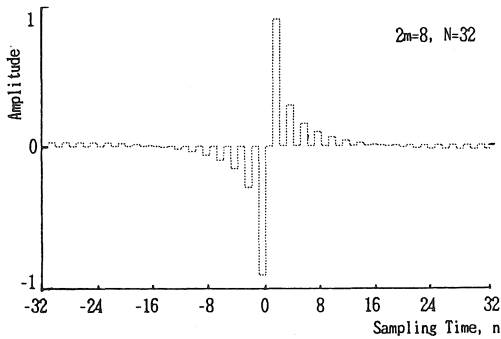
$$I_s(n) = \begin{cases} \frac{2}{N} \frac{\sin(2\pi n/N)}{1-\cos(2\pi n/N)} \frac{\sin(\pi n/N)}{\pi n/N} \\ = \frac{2\cos(\pi n/N)}{\pi n}, & \text{if } n \text{ is odd} \\ 0, & \text{if } n \text{ is even} \end{cases} \quad (11)$$

Eq.11 shows the ideal unit sample response of the Hilbert transformer, because the frequency domain Hilbert transform operator of eq.7 does exclude all of the processing error and because the Nyquist window with infinite length acts as an ideal low-pass filter as shown in the factor of Nyquist window $\sin(\pi n/N)/(\pi n/N)$.

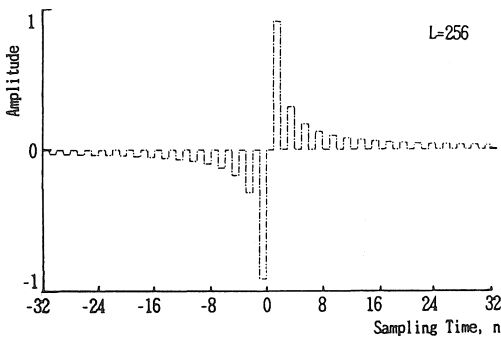
Equation 12 gives the unit sample response $I_m(n)$ of Rabinor's minmax FIR Hilbert (ab. in minmax) transformer[1].

$$I_m(n) = \begin{cases} \frac{2\sin^2(\pi n/2)}{\pi n} = \frac{1-\cos(\pi n)}{\pi n} \\ = \frac{2}{\pi n}, & \text{if } n \text{ is odd} \\ 0, & \text{if } n \text{ is even} \end{cases} \quad (12)$$

It is clearly shown in eqs.11 and 12 that the ST-DFT Hilbert transformer enhances minmax transformer. That is,



(a) ST-DFT Hilbert Transformer



(b) Minmax FIR Hilbert Transformer

Fig.3 Comparison of unit sample response between the ST-DFT and minmax Hilbert transformers

$$\lim_{N \rightarrow \infty} \text{Im} \{s(n)\} = \lim_{N \rightarrow \infty} \frac{2 \cos(\pi n/N)}{\pi n} = \frac{2}{\pi n} = \text{Im}(n), \quad (13)$$

here, n is odd.

5. RESULTS OF COMPUTER SIMULATIONS

The ST-DFT Hilbert transformer is substantiated through computer simulations both of unit sample response and phase shifting. All the simulations were carried on the CRAY X-MP of AIT to avoid roundoff error from calculation.

Figure 3 shows evident difference between unit sample response of ST-DFT Hilbert transformer (a) and that of minmax one (b). Here, the length L of FIR filter of minmax Hilbert transformer is set to be 256. The frame number $2m$ and frame length N of the ST-DFT transformer are set to be 8 and 32. The total length of the ST-DFT window $h(*)$, therefore, becomes 256 ($2mN=8 \times 32$) the same to minmax FIR filter.

As shown in fig.3(a), the unit sample response of ST-DFT transformer features of oscillation of its envelope being coincident with that of minmax transformer shown in fig.3(b). This oscillation of the envelope is induced with the $\cos(\pi n/N)$ factor of eq.11.

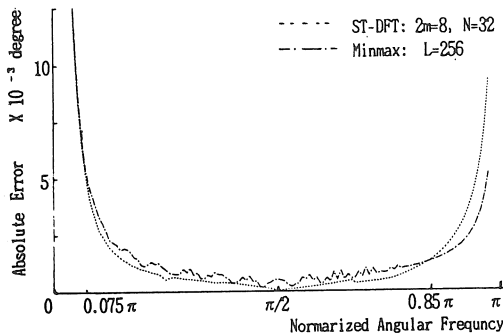


Fig.4 Phase shifting absolute error of the ST-DFT and minmax Hilbert transformers

That is, the response of ST-DFT transformer oscillates on all the $2mN$ sampling time with N period. On the other hand, minmax transformer response is non periodic on all the L sampling time.

This periodicity of the ST-DFT transformer improves phase shifting function in accuracy. Figure 4 shows phase shifting errors both of the ST-DFT and minmax transformer for tonal input signals. Where, the length $2mN$ and L are equally taken to be 256 and output signals are both analyzed by 256 frame length ST-DFT.

The ST-DFT transformer error indicated in fig.4 by dotted line is observed as $2m=8$ and $N=32$. The ST-DFT transformer does not exceed beyond the phase shifting error of minmax transformer also shown in fig.4 by chained line on the frequency domain of less than 0.85π ($= 3.4\text{kHz}$ of 8kHz sampling) and guarantees that the phase shifting error is within 5×10^{-3} degree for the practical frequency domain of more than 0.075π ($= 0.3\text{kHz}$ of 8kHz sampling) less than 0.85π .

CONCLUSION

Putting emphasis on the instantaneous spectrum signal processing, a noble Hilbert transformer was discussed through its circuitry configuration, unit sample response and phase shifting function. In spite of adopting a primitive truncated Nyquist for the significant window $h(*)$, ST-DFT Hilbert transformer can exceed Rabiner's minmax one in both phase shifting accuracy and rapidness of transient response. Farther studies will improve such primitive instantaneous spectrum signal processing as ST-DFT, ST-DFT Hilbert transformer, etc.

REFERENCES

- (1) L. R. Rabiner and R. W. Schafer, "On the behavior of minmax FIR digital Hilbert transformers", BSTJ, Vol.53, No.2, Feb.1974, PP.363 ~390
- (2) K. Daikoku and K. Suwa, "RZ SSB Transceiver with Equal-Gain Combiner for Speech and Data Transmission", GLOBECOM'88, Nov.28-Dec.1, 1988, Fort Lauderdale, FL, PP.26-4-1 ~ 26-4-5
- (3) M. Kishi, "A Proposal of Short Time DFT Hilbert Transformers and its Configuration", the Transactions of IEICE, Vol.E71, No.5, May 1988, PP.466 ~468
- (4) M. Kishi, "The Properties and Configuration of the Short Time DFT Hilbert Transformers", IEEE International Conference on Acoustics, Speech, and Signal Processing (ICASSP89), 23-26 May, 1989, Glasgow, Scotland, Proceedings ICASSP89 Vol.2, Speech Processing 2, Digital Signal Processing, No.D4.10, PP.1019-1022

(受理 平成2年3月20日)